

ME729 Advanced Robotics - PID and Linear Control

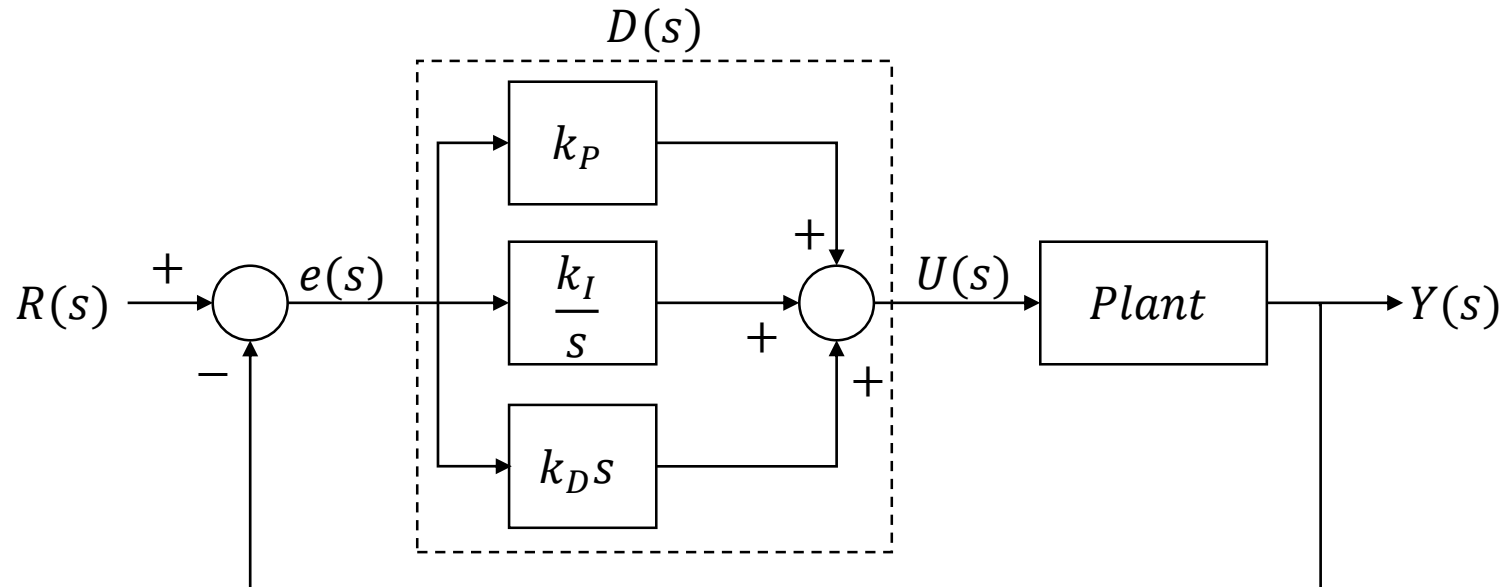
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PID and Linear Control

□ PID controller

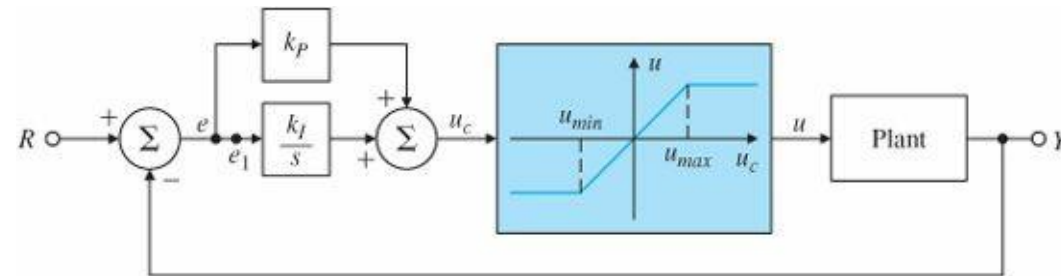
- Proportional–Integral–Derivative controller.
- $D(s) = k_P + \frac{k_I}{s} + k_D s$



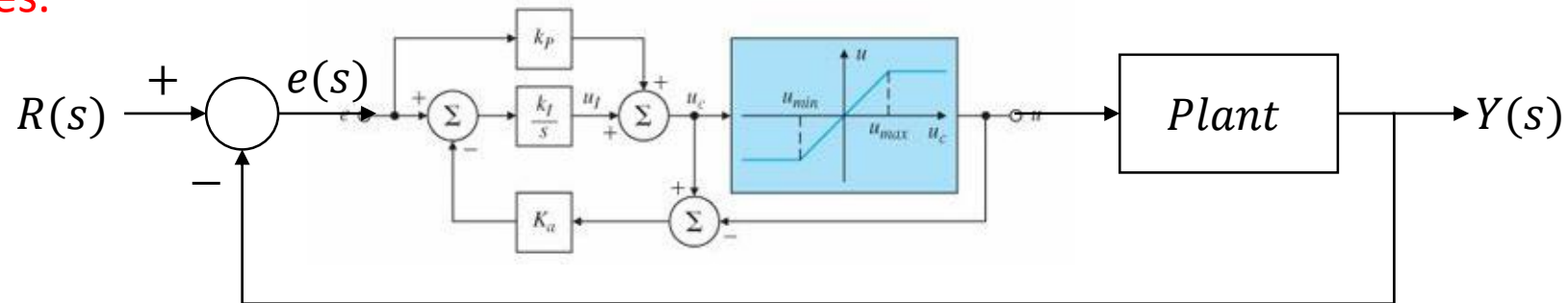
- The PID controller is broadly applicable, since it relies only on the response of the measured process variable, **not on knowledge or a model of the underlying process**.
- The PID gain tuning is a difficult problem.
- There are several methods for tuning the gains: manual tuning, Ziegler-Nichols method, etc.

PID and Linear Control

□ PID controller - Integrator antiwindup



- Suppose a given reference step is more than large enough to cause the actuator to saturate at u_{max} .
- The integrator continues integrating the error e , and the signal u_c keeps growing.
- However, the input to the plant is stuck at its maximum value, namely $u = u_{max}$, so the error remains large until the plant output exceeds the reference and the error changes sign.
- **The solution to this problem is an integrator antiwindup, which “turns off” the integral action when the actuator saturates.**

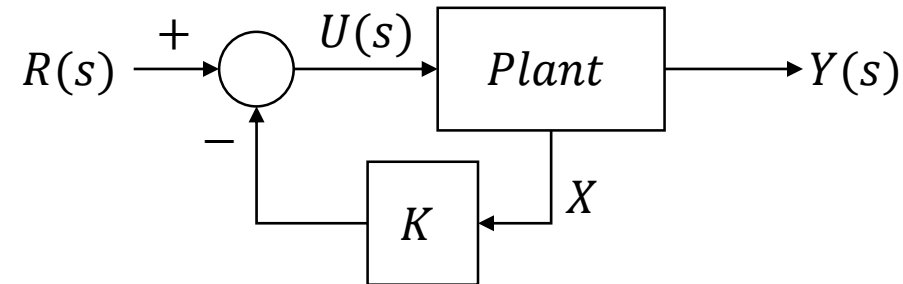


- In this scheme, as soon as the actuator saturates, the feedback loop around the integrator becomes active and acts to keep the input to the integrator at e_1 small.

PID and Linear Control

□ Pole-placement method

- To place the closed-loop poles of a plant in pre-determined locations (desired poles) in the s-plane.



- If the closed-loop dynamics can be represented by the state space equation with output equation,

$$\dot{X} = AX + BU, \quad Y = CX$$

then the poles of the system transfer function are the roots of the characteristic equation given by

$$\det(sI - A) = 0$$

Consider an input proportional to the state vector,

$$U = -KX$$

Substituting into the state space equations above,

$$\dot{X} = (A - BK)X$$

Therefore, the poles of the full state feedback system are given by $\det[sI - (A - BK)] = 0$.

- Determine feedback gain, K , through comparing the poles of the full state feedback system with desired poles.

PID and Linear Control

□ Pole-placement method – continued

- For example, there is a control system given by the following state space equations

$$\dot{X} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} X + \begin{bmatrix} 0 \\ 1 \end{bmatrix} U$$

- Desire poles: $s = -1$, and $s = -5$

→ The desired character equation is $(s + 1)(s + 5) = s^2 + 6s + 5 = 0$.

- Let $K = [k_1 \ k_2]$,

$$|sI - (A - BK)| = \det \begin{bmatrix} s & -1 \\ 2 + k_1 & s + 3 + k_2 \end{bmatrix} = s^2 + (3 + k_2)s + (2 + k_1)$$

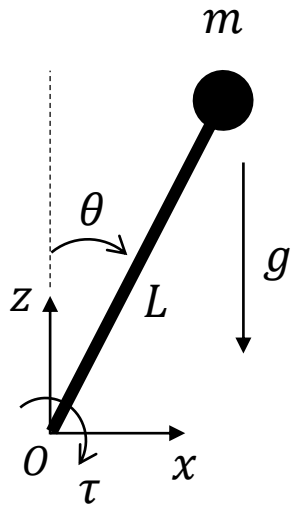
- Comparing two equations,

$$s^2 + 6s + 5 = s^2 + (3 + k_2)s + (2 + k_1)$$

- Therefore, $k_1 = 3$, and $k_2 = 3$.

PID and Linear Control

□ Inverted pendulum model (IPM)



- For IPM, the kinetic and potential energies are

$$K = 1/2 mL^2 \dot{\theta}^2$$

$$P = mgL \cos \theta$$

- The Lagrangian

$$L = K + P = 1/2 mL^2 \dot{\theta}^2 + mgL \cos \theta$$

- Lagrangian's equation

$$\frac{\partial L}{\partial \dot{\theta}} = mL^2 \dot{\theta}$$

$$\frac{d}{dt} \frac{\partial L}{\partial \dot{\theta}} = mL^2 \ddot{\theta}$$

$$\frac{\partial L}{\partial \theta} = -mgL \sin \theta$$

$$\therefore \tau = mL^2 \ddot{\theta} - mgL \sin \theta$$

PID and Linear Control

□ Inverted pendulum model (IPM) – continued

- Linearization:

Assume that θ is small. Then, $\sin \theta \approx \theta$ and $\cos \theta \approx 1$.

After linearizing Lagrangian's equation,

$$\therefore \tau = mL^2\ddot{\theta} - mgL\theta$$

- State-space representation:

Rewrite the linearized equation,

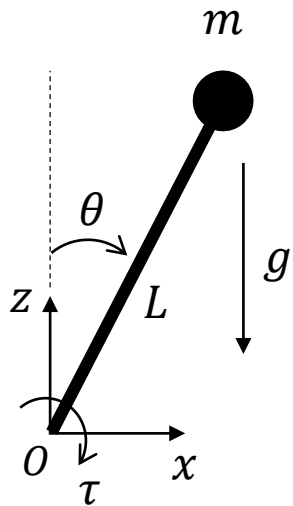
$$\ddot{\theta} = \frac{g}{L}\theta + \frac{1}{mL^2}\tau$$

Then,

$$\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{g}{L} & 0 \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{mL^2} \end{bmatrix} \tau$$

Set state as $X = [\theta \quad \dot{\theta}]^T$, input u as the joint torque τ ,

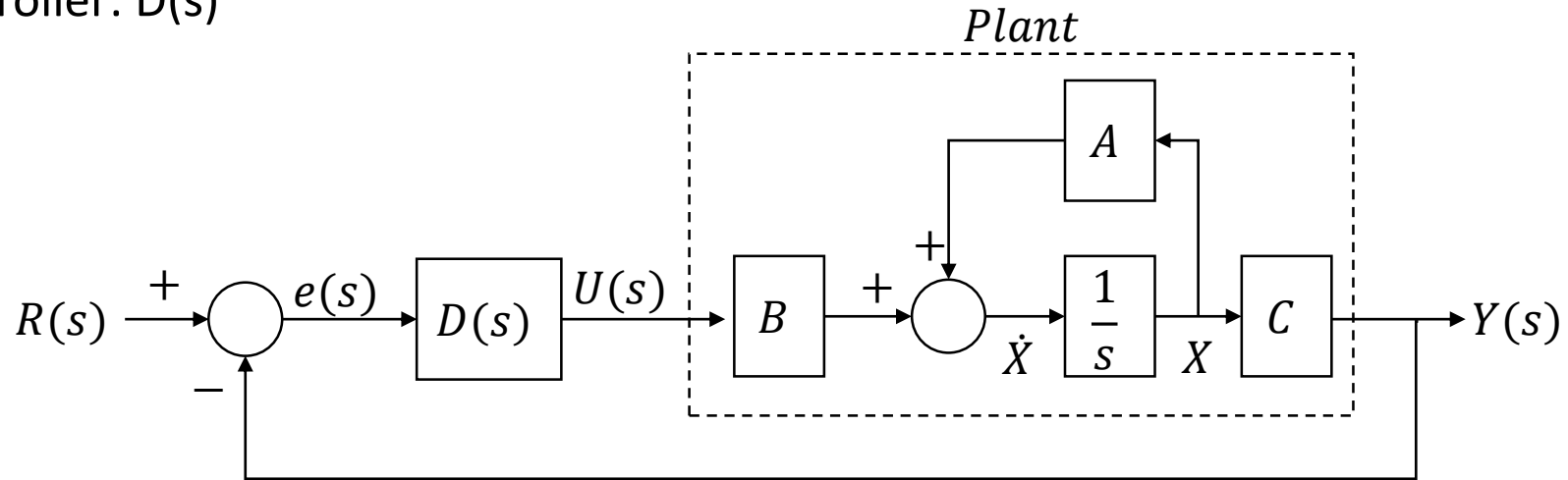
$$A = \begin{bmatrix} 0 & 1 \\ \frac{g}{L} & 0 \end{bmatrix}, B = \begin{bmatrix} 0 \\ \frac{1}{mL^2} \end{bmatrix}, \text{ and } C = [1 \quad 0].$$



PID and Linear Control

□ Inverted pendulum model (IPM) – continued

- PID controller: $D(s)$



- Pole-placement method

